Commonwealth of Kentucky Division for Air Quality

PERMIT STATEMENT OF BASIS

Draft Synthetic Minor Permit No. VF-02-001 (Revision 2)
Catlettsburg Refining, L.L.C.
Catlettsburg, KY
February 10, 2004
GAURAV SHIL, Reviewer
Plant I.D. # 021-019-00004
Application Log # 55330

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I. DESCRIPTION OF THE PROPOSED MODIFICATION

The site of the proposed project is the petroleum refinery operated by Catlettsburg Refining, LLC, a subsidiary of Marathon Ashland Petroleum LLC. This refinery is located on the Big Sandy River in Catlettsburg, Boyd County, Kentucky.

The refinery modernization project involves installation of new emissions units, modifications to some existing emissions units, and removal of some existing emissions units. This will allow the refinery to produce cleaner-burning transportation fuels, to improve yields, to utilize a wider range of purchased feed materials, and to reduce fixed and operating costs. In addition, the project will substantially reduce emissions of sulfur dioxide and nitrogen oxides from the refining operations.

Synthetic minor construction permit number VF-02-001 was issued for this project on March 29, 2002. On-site construction commenced during the first week of April. Permit number VF-02-001 was revised on July 25, 2003. Project completion is anticipated to occur no later than September 2005.

PROPOSED CHANGES WITH LOG# 56022

Permit number VF-02-001 (Revision 2) covers minor changes to the requested synthetic minor emission limits contained in permit number VF-02-001, issued in March 2002, as well as requested changes to permit terms relating to monitoring and testing requirements. The project will not result in a significant net emissions increase for any regulated air pollutant. Thus, the Prevention of Significant Deterioration (PSD) regulations codified at 401 KAR 51:017 and the major nonattainment area NSR regulations codified at 401 KAR 51:052 are not applicable. The proposed changes at the refinery include the following:

1. CHANGE OF SYNTHETIC MINOR EMISSION LIMITS

The synthetic minor emission limits for the following units have been revised. As shown in Emissions Analysis, these changes have been incorporated into the PSD netting analysis, and do not cause the refinery modernization project to become a major modification.

a. Fluidized Catalytic Cracking Unit (ID No. 2-116-B)

The synthetic minor NOx emission limit for the Fluidized Catalytic Cracking Unit is revised from 237.0 tons per year to 365.0 tons per year.

b. No. 4 Vacuum Charge Heaters (ID No. 2-26-B-2 and 2-23-B-6)

The heat input limit for the 2-26-B-2 heater is revised from 138 MMBtu/hr to 112 MMBtu/hr. The synthetic minor emission limits for the 2-26-B-2 heater reflect the decreased heat

input capacity. The new and old (in parenthesis) synthetic minor emission limits are listed in the following table.

Affected Units		Maximum emissions (tons/yr)								
Affected Clifts	SO2	NOx	VOC	CO	PM_{10}					
No. 4 Vacuum Charge Heater	15.1	39.9	3.1	47.1	4.3					
(2-26-B-2)	(16.2)	(42.8)	(3.3)	(50.6)	(4.6)					

from

c. HPVGO Hydrotreater Heaters (ID No. 2-104-B-1 and 2-104-B-2)

The synthetic minor NOx emission limit for both HPVGO Hydrotreater Heaters is revised 19.5 tons per year to 23.8 tons per year.

2. CHANGES TO PERMIT TERMS

In addition to changes in the synthetic minor emission limits, existing permit terms for combustion devices have been revised. Catlettsburg Refining, LLC proposed to use CEMS for large, controlled units. Also, CRLLC proposed to relax the method of compliance demonstration for NOx and CO synthetic minor emission limits for several other combustion devices. The Division determined that each of these combustion devices has a potential to emit (PTE) for NOx and CO that is very close to the synthetic minor permit emission limits. CRLLC calculates for each day, in tons per year, the rolling 365-day emissions of each pollutant and maintain daily records of daily heat input rate and 365-day rolling sum heat input rate to the combustion devices. CRLLC also calculates and maintains daily records of 365-day rolling sum emissions of each pollutant from the combustion devices. Permit number VF-02-001 (Revision 1) contains an hourly heat input capacity operating limit for each combustion device. CRLLC determines the Gross Calorific Value of the fuel combusted by using ASTM methods on a weekly basis. CRLLC measures the rate of fuel burned for each fuel daily or at shorter intervals. Based on the above mentioned requirements in the Permit, the Division proposed the following changes in the method of compliance demonstration for the combustion devices:

A. Compliance Demonstration Method for NOx emission limit

MAP Unit No.	Heater Description	Date commenced	Heat input capacity (mmBTU/hr)	Existing compliance demonstration method	DAQ proposed method
1-2-B-3	#2 Crude Charge Htr	1977	99	CEMS	Stack Test
2-23-B-3	#3 Crude Unit Htr	1972	161	CEMS	CEMS
2-23-B-4	#3 Crude Unit Htr	1972	161	CEMS	CEMS
2-30-B-1	Saturate Gas	1972	162	CEMS	CEMS

	Plant Heater				
2-122-B-1	Reformer Heater	2002	365	CEMS	CEMS
2-116-B-1, 2-116-B-2	FCCU CO Boilers	1980	784	CEMS	CEMS
MAP Unit No.	Heater Description	Date commenced	Heat input capacity (mmBTU/hr)	Existing compliance demonstration method	DAQ proposed method
2-121-B-1	DD #2 Reactor Charge Htr	1993	55	CEMS	Stack Test
2-121-B-2	DD #2 Reactor Charge Htr	1993	55	CEMS	Stack Test
2-121-B-3	DD #2 Stripper Reboiler	1993	85	CEMS	Stack Test
2-26-B-2	#4 Vacuum Charge Htr	1995	125	CEMS	Stack Test
2-23-B-6	#4 Vacuum Charge Htr	1977	165	CEMS	Stack Test
2-104-B-1	HPVGO Hydrotreater Charge Htr	1976	90	CEMS	Stack Test
2-104-B-2	HPVGO Hydrotreater Charge Htr	1976	90	CEMS	Stack Test
2-103-B-1	LPVGO Hydrotreater Charge Htr	1975	45	CEMS	Stack Test
2-103-B-2	LPVGO Hydrotreater Charge Htr	1975	45	CEMS	Stack Test
2-103-B-3	LPVGO Hydrotreater Charge Htr	1975	50	CEMS	Stack Test
2-36-B-1	HF Alky Isostripper Reboiler	1978	86	CEMS	Stack Test

B. Compliance Demonstration Method for CO emission limit

MAP Unit No.	Heater Description	Date commenced	Heat input capacity (mmBTU/hr)	Existing compliance demonstration method	DAQ proposed method
1-2-B-3	#2 Crude Charge Htr	1977	99	Stack Test	Stack Test
2-23-B-3	#3 Crude Unit Htr	1972	161	Stack Test	CEMS
2-23-B-4	#3 Crude Unit Htr	1972	161	Stack Test	CEMS
2-30-B-1	Saturate Gas Plant Heater	1972	162	AP-42	CEMS
2-122-B-1	Reformer Heater	2002	365	Stack Test	CEMS
2-116-B-1, 2-116-B-2	FCCU CO Boilers	1980	784	CEMS	CEMS
2-121-B-1	DD #2 Reactor Charge Htr	1993	55	Stack Test	AP-42
2-121-B-2	DD #2 Reactor Charge Htr	1993	55	Stack Test	AP-42
2-121-B-3	DD #2 Stripper Reboiler	1993	85	Stack Test	AP-42
2-26-B-2	#4 Vacuum Charge Htr	1995	125	Stack Test	Stack Test
2-23-B-6	#4 Vacuum Charge Htr	1977	165	Stack Test	Stack Test
2-104-B-1	HPVGO	1976	90	Stack Test	Stack Test

	Hydrotreater Charge Htr HPVGO				
2-104-B-2	Hydrotreater Charge Htr	1976	90	Stack Test	Stack Test
2-103-B-1	LPVGO Hydrotreater Charge Htr	1975	45	Stack Test	Stack Test
2-103-B-2	LPVGO Hydrotreater Charge Htr	1975	45	Stack Test	Stack Test
MAP Unit No.	Heater Description	Date commenced	Heat input capacity (mmBTU/hr)	Existing compliance demonstration	DAQ proposed method
		_	(IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	method	method
2-103-B-3	LPVGO Hydrotreater Charge Htr	1975	50	method Stack Test	Stack Test

PROPOSED CHANGES WITH LOG# 55330

This permit covers minor changes to the refinery modernization project scope that have occurred subsequent to the issuance of Synthetic minor construction permit number VF-02-001 on March 29, 2002, as well as changes to permit terms relating to monitoring requirements. As documented in permit number VF-02-001, the project will not result in a significant net emissions increase for any regulated air pollutant. Thus, the Prevention of Significant Deterioration (PSD) regulations codified at 401 KAR 51:017 and the major nonattainment area NSR regulations codified at 401 KAR 51:052 are not applicable. The proposed changes at the refinery include the following:

1. HYDROGEN GENERATION UNIT

A new process unit to be installed at the refinery is a Hydrogen Generation Unit (ID No. 2-122). The Hydrogen Generation Unit, its reformer vent, and the associated Reformer Heater (ID No. 2-122-B-1) are covered by the existing permit number VF-02-001. The existing permit number VF-02-001 is based on a nominal Hydrogen Generation Unit hydrogen production capacity of 30 million scf/day and a maximum allowable Reformer Heater heat input rate of 310 MMBtu/hr (lower heating value, LHV). The final, detailed engineering of the Hydrogen Generation Unit has resulted in two changes to the design of this unit: The nominal production capacity has increased to 34 million scf/day, and a dedicated emergency flare has been added. In addition, a dedicated cooling tower serving the Hydrogen Generation Unit has

been added to the scope of the refinery modernization project. As a result of these changes, several permit terms are revised.

2. HF ALKY UNIT

The refinery modernization project scope has been expanded to include the addition of an HF Alky Hot Oil Heater (ID No. 2-36-B-2). This heater will be fired with natural gas and refinery fuel gas and will have a maximum heat input capacity of 18 MMBtu/hr (LHV). Permit terms allowing the installation of this heater are included in the revision.

3. DISTILLATE STORAGE TANKS

The refinery modernization project scope has been expanded to include the addition of four distillate storage tanks (Nos. 910, 911, 912, 913). Each tank will be equipped with an internal floating roof. Permit terms allowing the installation of these tanks are included in the revision.

4. CHANGES TO PERMIT TERMS

Catalytic Cracking Unit has been deleted.

In addition to inclusion of new permit terms, existing permit terms for combustion devices, hydrotreaters, desulfurizers, storage vessels and Fluidized Catalytic Cracking Unit have been revised. Section G a) 16, General Compliance Requirements has been removed with this revision. General conditions for combustion devices, Specific monitoring requirement 2.D. has been deleted from VF-02-001 (Revision 1) because all combustion devices listed in Section B are not required to install NOx CEMS to demonstrate compliance with the synthetic minor NOx emission limits. Pursuant to comments from Ashland Regional office, Operating Limitation 1.D.iii. for New Fluidized

The Division was processing the request related to requirement of CEMS and stack tests for various combustion devices. Pursuant to the request of the Permittee, in order to expedite the permitting process, the decision related to CEMS and stack test requirements is not made with this permitting step.

PROPOSED CHANGES WITH LOG# 53771

The only new process unit to be installed at the refinery is a Hydrogen Generation Unit (ID No. 2-122) with a nominal hydrogen production capacity of 30 million scf/day. The increased hydrogen supply is necessary for the increased hydrotreating capacity, which in turn is necessary for production of low-sulfur gasoline. The Hydrogen Generation Unit will include a fired Reformer Heater (ID No. 2-122-B-1).

One new storage vessel, Tank 920, will be installed. This tank will have a capacity of 150,000 barrels and will store gas oil.

The refinery process units to be modified are as follows:

The No. 2 Crude Unit (ID No. 1-2) will be modified to increase its nominal throughput capacity to 30,000 barrels per day. The existing heater within this unit (No. 2 Crude Charge Heater, ID No. 1-2-B-3) will not be modified.

The No. 3 Crude Unit (ID No. 2-23) will be modified to increase its crude slate flexibility, product recovery, and energy efficiency. The nominal capacity will be increased from 130,000 to 145,000 barrels per day. The heaters within this unit (No. 3 Crude Charge Heater #1, ID No. 2-23-B-3, and No. 3 Crude Charge Heater #2, ID No. 2-23-B-4) will be modified to increase heat input capacity, improve efficiency, and reduce NO_X emissions.

The No. 4 Vacuum Unit (ID No. 2-26) will be modified to increase its product recovery and energy efficiency and to increase its nominal capacity from 38,000 to 75,000 barrels per day. The existing heater within this unit (No. 4 Vacuum Charge Heater, ID No. 2-26-B-2) will not be modified. The existing FCC Charge Heater (currently ID No. 2-1-B-8) will be switched to the No. 4 Vacuum Unit and will operate in parallel with the existing No. 4 Vacuum Charge Heater and renamed as the No. 4 Vacuum Charge Heater (ID No. 2-23-B-6). This heater will be modified to increase its heat input capacity.

The existing Vacuum Gas Oil Hydrotreater (ID No. 2-104) will be modified to increase its nominal capacity from 40,000 to 60,000 barrels per day. This unit will be renamed the High-Pressure Vacuum Gas Oil (HPVGO) Hydrotreater. The heaters within this unit (HPVGO Charge Heater No. 1, ID No. 2-104-B-1, and HPVGO Charge Heater No. 2, ID No. 2-104-B-2) will not be modified, but will be retrofitted with low-NO $_{\rm X}$ burners.

The existing Kerosene Desulfurizer (ID No. 2-103) will be converted to a gas oil hydrotreater with a nominal capacity of 40,000 barrels per day. This unit will be renamed the Low-Pressure Vacuum Gas Oil (LPVGO) Hydrotreater. The two reactor charge heaters within this unit (LPVGO Charge Heater No. 1, ID No. 2-103-B-1 and LPVGO Charge Heater No. 2, ID No. 2-103-B-2) will not be modified. The LPVGO Stripper Heater (ID 2-103-B-3) will be converted from a stripper reboiler to a stripper charge heater.

The existing Residual Catalytic Cracking (RCC) Unit (ID No. 2-109) will be expanded and converted to a Fluidized Catalytic Cracking (FCC) Unit with a nominal gas oil charge capacity of 95,000 barrels per day. Four condensing turbine drivers and the associated air blowers and wet gas compressors will be replaced with a single electric motor-driven air blower and a single electric motor-driven wet gas compressor to improve process flexibility and energy efficiency. The FCC Unit catalyst regenerator also will be modified and expanded.

The heat recovery units (Unit ID Nos. 2-116-B-1 and 2-116-B-2) associated with the converted FCC Unit will be retrofitted with low- NO_X burners, and one of the two units will be retrofitted with a selective non-catalytic reduction (SNCR) system. At each of these units, the internal grid will be removed and the steam turbines serving the forced-draft fans will be replaced with electric motors. The existing limestone scrubber serving the heat recovery units will be eliminated, as deep hydrotreating of FCC Unit feedstock will eliminate the need for further SO_2 control. (Provisions will be made to add a de- SO_x catalyst additive, should it be required, in order to meet the SO_2 emission limit.)

The Gas Concentration Plant (Unit ID No. 2-110) associated with the converted FCC Unit (ID No. 2-109) will be upgraded and expanded, including extensive piping modifications. This unit does not include any fired heaters.

The existing Distillate Desulfurizer (ID No. 2-121) will be modified to increase its nominal capacity from 55,000 to 75,000 barrels per day. The heaters within this unit (DDS Reactor Charge Heater No. 1, ID No. 2-121-B-1; DDS Reactor Charge Heater No. 2, ID No. 2-121-B-2; and DDS Stripper Reboiler, ID No. 2-121-B-3) will not be modified.

The existing Sulfur Recovery Plant (ID Nos. 2-106 and 2-120) will be modified to improve reliability and efficiency and to increase nominal capacity from 400 long tons per day to 600 long tons per day.

The No. 2 Vacuum Unit (ID No. 1-2), including the associated charge heater (ID No. 1-2-B-1), will be permanently removed from service.

The existing Fluidized Catalytic Cracking Unit (ID No. 2-1), including the associated CO boiler (ID No. 2-601-B-9) and electrostatic precipitator, will be permanently removed from service.

II. EMISSION ANALYSIS

A. Information Given and Assumed

All information used in making this determination was derived from the permit application and supplemental information provided by Catlettsburg Refining, L.L.C.

B. Emission Summaries and Calculation Methods

In accordance with KDAQ and U.S. EPA policy, the net emissions increase for each pollutant is calculated using the process set forth in the *New Source Review Workshop Manual: Prevention of Significant Deterioration and Nonattainment Area Permitting* U.S. EPA, Office of Air Quality Planning and Standards. Research Triangle Park, NC Draft, October 1990. The emissions increase calculations include emissions from new and modified emissions units as well as other affected emissions units upstream and downstream of the new and modified equipment. Emissions increases for all modified and debottlenecked emissions units are calculated using a past-actual-to-future-potential methodology.

For PM/PM_{10} , SO_2 , NO_X , CO, and VOC emissions, netting analyses were performed, including all contemporaneous emissions increases and decreases. For all pollutants, the net emissions increases are less than significant (in fact, for PM/PM_{10} , SO_2 , NO_X , and CO, the project will result in decreases).

Summary of Tables used for Emission Calculations

The emission calculations are summarized in the following tables. Specifically:

- ?? Table 1 provides a listing of emission units affected by the proposed project and a summary of the emissions increase or decrease from each affected unit.
- ?? Table 2 provides pre-modification actual emissions for the 24-month period June 1999 through May 2001 for each modified or debottlenecked emission unit.
- ?? Table 3 provides post-modification potential emissions for each modified or debottlenecked emission unit. These values are equivalent to the permitted emission limits included in Section B of the draft permit.
- ?? For each unit that is neither modified nor debottlenecked, Table 4 provides the incremental emissions increase.
- ?? Table 5 provides the netting analyses, including all contemporaneous emissions increases and decreases.

				emissions	changes	Γ		
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	voc	СО	PM10	comments
1-2	n/a	#2 Vacuum Unit			-6.4			Unit will be shut down. Emissions decreases represent baseline
1-2-B-1	B019	#2 Vacuum Charge Htr	-0.1	-5.5	-0.3	-4.6	-0.4	actual emissions.
1-2	n/a	#2 Crude Unit			0.1			Unit will undergo minor piping modifications. Emissions increases represent incremental change in component count.
1-2-B-3	B018	#2 Crude Charge Htr	-195.5	3.4	1.3	19.9		Heater may be debottlenecked. Emissions increases represent difference between maximum allowable emissions and 1999- 2001 actual emissions.
2-1	n/a	(Old) FCC Unit			-78.4	-615.5		Unit will be shut down. (Charge heater is changing service and being moved to the #4 vacuum
2-1-B-8	B060	(Old) FCC Charge Htr	-0.5	-87.2	-1.7	-26.1	-2.4	unit. For emissions increase purposes, this change is treated as a new installation - see below.)
2-601-B-9	B017	(Old) FCC CO Boiler	-3,193.0	-387.0	-6.8	-160.9	-115.6	Emissions decreases represent baseline actual emissions.
2-2	n/a	(Old) FCC Gas Con Unit			-55.6			Equipment and components will be removed. Emissions decreases represent incremental change in component count.
2-23	n/a	#3 Crude Unit			9.9			Unit will undergo piping modifications. Emissions increases represent incremental change in component count.

		Tal	ble 1. Summar	y of Emissi	ons Char	nges		
MAP Unit #	KEIS Unit #	Affected Units	SO2	emissions (PM10	and a second	
Unit #	Unit #	Affected Units	502	NOx	VOC	CO	PM10	comments
2-23-B-3	B004	#3 Crude Unit Htr	19.6	-139.9	0.5	6.9	9 0.6	Heaters may be debottlenecked. Emissions increases represent difference between maximum
2-23-B-4	B005	#3 Crude Unit Htr	1.0	-136.3	0.5	8.0	0.7	allowable emissions and 1999- 2001 actual emissions.
2-26		#4 Vacuum Unit			3.3			Unit will undergo piping modifications. Emissions increases represent incremental change in component count.
2-26-B-2		#4 Vacuum Charge Htr	10.5	5.0	0.4	5.9	9 0.5	Heater may be debottlenecked. Emissions increases represent difference between maximum allowable emissions and 1999- 2001 actual emissions.
2.22 P. 6		#4 Vacuum Charge Litr	24.4	444.2	4.4	66.0		Treated as a new emissions unit for calculation purposes - emissions increases represent maximum allowable emissions. (Was formerly the FCC charge heater and was treated as "shut down" in the FCC Unit - see
2-23-B-6		#4 Vacuum Charge Htr	21.4	111.3	4.4	66.8	5 6.0	above.)
2-30		Saturate gas plant						Unit may be debottlenecked. No change in piping or fugitive emissions.
2-30-B-1	B010	Saturate gas plant heater	20.1	-77.4	1.7	25.9	2.3	Heater ma be debottlenecked. Emissions increases represent difference between maximum allowable emissions (see "PTE" table for details) and baseline

		Tab	le 1. Summai	y of Emissi	ons Char	nges		
				emissions	changes	(tons/yr)	I	
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	VOC	СО	PM10	comments
								actual emissions (see "baseline" table for details)
2-36	n/a	HF Alky Unit						Unit may be debottlenecked. No change in piping or fugitive emissions.
2-36-B-1	B065	HF Alky Isostripper Reboiler	10.8	3 25.7	1.3	20.1	1.8	Heater may be debottlenecked. Emissions increases represent difference between maximum allowable emissions and 1999- 2001 actual emissions.
2-122	n/a	Hydrogen Generation Unit			14.5			New installation. Includes reformer vent. No equipment in VOC service.
2-122-B-1	n/a	Reformer Heater	1.1	104.6	9.7	70.3	3 13.3	New installation. Emissions increases represent proposed maximum allowable emissions.
2-103	n/a	Low Pressure VGO Hydrotreater			14.1			Unit will undergo piping modifications. Emissions increases represent incremental change in component count.
2-103-B-1	B043	LPVGO Hydrotreater Charge Htr	5.4	19.6	1.1	16.3	3 1.5	Heaters may be debottlenecked. Emissions increases represent
2-103-B-2	B044	LPVGO Hydrotreater Charge Htr	2.0	4.5	0.1	2.2	0.2	difference between maximum
2-103-B-3	B045	LPVGO Hydrotreater Stripper Htr	4.7	7 16.2	0.8	12.9	1.2	2001 actual emissions
2-104	n/a	High Pressure VGO Hydrotreater			89.3			Unit will undergo piping modifications. Emissions increases represent incremental change in component count.

		Tab	le 1. Summar	y of Emissi	ons Char	nges		
MAP	KEIS			emissions o				
Unit #	Unit #	Affected Units	SO2	NOx	VOC	CO	PM10	comments
2-104-B-1	B046	HPVGO Hydrotreater Charge Htr	6.5	-32.2	0.9	13.7	1.2	Heaters may be debottlenecked. Emissions increases represent difference between maximum
2-104-B-2	B047	HPVGO Hydrotreater Charge Htr	6.2	-42.1	0.8	12.2	1.1	allowable emissions and 1999- 2001 actual emissions.
2-106-B-307	B042	No. 1 SRU Thermal Oxidizer	144.2	7.9	0.4	6.6	0.6	Units may be debottlenecked by hydrotreater installations. Emissions increases represent
2-120-B-2	n/a	No. 2 SRU Thermal Oxidizer			0.5			difference between maximum allowable emissions and 1999-2001 actual emissions.
2-106 & 2-107	n/a	#1 Sulfur Plant						No change in component count.
2-118, 2-119 & 2-120	n/a	#2 Sulfur Plant						, .
2-109	n/a	(New) FCC Unit			8.6			Unit will undergo extensive piping modifications. Emissions increases represent incremental change in component count.
2-116-B-1, 2-116-B-2	B066, B067	(New) FCCU Heat Recovery Units North and South	-793.0	-133.0	38.2	415.9	46.0	Unit will undergo extensive modifications. Emissions increases represent difference between maximum allowable emissions and 1999-2001 actual emissions.
2-110	n/a	(New) FCC Gas Con Unit			16.0			Unit will undergo extensive piping modifications. Emissions increases represent incremental change in component count.

		Tab	ole 1. Summa	ry of Emissi	ons Chai	nges		
MAP Unit #	KEIS Unit #	Affected Units	SO2	emissions NOx		comments		
2-121	n/a	Distillate desulfurizer #2	002	IVOX	4.4	CO	PM10	Unit will undergo piping modifications. Emissions increases represent incremental change in component count.
2-121-B-1	B066	DD #2 Reactor Charge Htr	6.9	9 6.9	0.9	13.	_	Heaters may be debottlenecked. Emissions increases represent
2-121-B-2	B067	DD #2 Reactor Charge Htr	6.9	6.9	0.9	13.		difference between maximum
2-121-B-3	B068	DD #2 Stripper Reboiler	10.3	3.0	0.2	2.	8 0.3	2001 actual emissions.
		Hydrogen plant cooling tower					0.4	New installation. Emissions increases represent proposed maximum allowable emissions.
		Hydrogen plant emergency flare		0.1	0.3	0.8		New installation. Emissions increases represent proposed maximum allowable emissions.
n/a	n/a	tankage			17.4			
Tank 701	HJ	gas oil			0.0)		Tanks may be debottlenecked.
Tank 702	HK	gas oil			0.0			Emissions increases represent difference between maximum
Tank 845	LX	gas oil			0.0			allowable emissions and 1999- 2001 actual emissions.
Tank 821	LH	gas oil			0.0			
Tank 733	IF	gas oil			4.6			
Tank 855	ME	gas oil			3.0			
Tank 81		gas oil			9.2			

		Tab	ole 1. Summai	y of Emissi	ons Char	nges		
				emissions	changes	(tons/yr)	1	
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	VOC	СО	PM10	comments
3 1	<u> </u>	- meeted Cime	002	ITOX	100		1 10110	Commonte
Tank 152	FD	gas oil			0.0			
Tank 734	IM	FCC gasoline			1.9			
Tank 783	JT	FCC gasoline			2.9			
Tank 856	JV	FCC gasoline			0.9			
Tank 910		Distillate			1.2			
Tank 911		Distillate			0.6			
Tank 912		Distillate			0.6			
Tank 913		Distillate			1.0			
Tank 920	n/a	swing tank			10.1			
4.45.4	D004	P-Chem Reformer Guard	0.0		0.0	0 -		Emissions increases represent the
1-4-B-1	B021	Case Htr	0.9	1			+	incremental increases due to higher throughput/utilization.
1-4-B-2,3,4	B022	P-Chem Reformer Htr	2.4	1				1
1-4-B-7,8	B050	Petrochem Reformer Htr	1.1		1		1	
1-44-B-1		LP CCR Charge Heater	0.9	1			1	
1-44-B-2		LP CCR No. 1 Interheater	1.1	+	1		1	-
1-44-B-3		LP CCR No. 2 Interheater	0.0	+			+	
1-44-B-4		LP CCR No. 3 Interheater	0.6	2.1	0.1	2.0	0.2	
1-44-B-5		LP CCR Debutanizer Reboiler	0.3	3 1.0	0.1	1 .	0.1	
1-44-D-3		C5/C6 Isomerization	0.3	1.0	0.1	1.0	0.1	
2-35-B-1, 2	B040	Heaters	1.0	3.2	0.2	3.0	0.3	3
2-101-B-1	B064A	Naphtha Hydrotreater Charge Heater	0.0					
2-101-B-2	B064B	Naphtha Hydrotreater Stripper Reboiler	1.0	3.3	0.2	3.1	0.3	3
2-102-B-1A	B109	HP CCR Reactor Heater	1.8	6.1	0.4	5.7	0.5	
2-102-B-1B	B110	HP CCR Reactor Heater	2.0	6.5	0.4	6.1	0.6	

		Tab	le 1. Summar	y of Emissi	ons Chai	nges		
				emissions (
MAP	KEIS							
Unit #	Unit #	Affected Units	SO2	NOx	VOC	CO	PM10	comments
2-102-B-1C	B111	HP CCR Reactor Heater	1.4	4.7	0.3	4.4	0.4	
2-102-B-1D	B112	HP CCR Reactor Heater	0.4	1.5	0.1	1.4	0.1	
		HP CCR Debutanizer						
2-102-B-2	B113	Reboiler	0.3	1.1	0.1	1.0	0.1	
		Total project increases (not						
		including decreases)	444.3	301.9	280.8	780.4	85.5	
		Significant level	40.0	40.0	40.0	100.0	15.0	
		Project significant / requires						
		netting	yes	yes	yes	yes	yes	

Table 2. Baseline Actual Emissions

		actual em	issions (to	ons/yr)		
Affected Units	SO2	NOx	voc	со	PM10	Comments
#2 Vacuum Unit			6.4			Emissions represent equipment leaks.
#2 Vacuum Charge Htr	0.1	5.5	0.3	4.6	0.4	Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
#2 Crude Charge Htr	208.3	44.3	1.3	20.2		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
(Old) FCC Unit			78.4	615.5		VOC emissions represent equipment leaks, including gas con unit. CO emissions represent periods of CO boiler bypass.
(Old) FCC Charge Htr	0.5	87.2	1.7	26.1	2.4	Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
(Old) FCC CO Boiler	3,193.0	387.0	6.8	160.9		Emissions represent 6/1999 - 5/2001 actual emissions, based on CEMS data where available.
(Old) FCC Gas Con Unit			55.6			VOC emissions represent equipment leaks.
#3 Crude Unit Htr	1.2	194.2	3.8	58.3	5.3	Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
#3 Crude Unit Htr	19.8	190.6	3.7	57.2		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
#4 Vacuum Charge Htr	4.6	34.8	2.7	41.2	3.7	Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
#4 Vacuum Charge Htr						Zero "baseline" emissions in this service. (6/1999 - 5/2001 actual emissions represented for service as the FCC charge heater - see above.)
HF Alky Isostripper Reboiler	0.3	15.7	1.0	14.7		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.

Table 2. Baseline Actual Emissions

		actual em	issions (to	ons/yr)	I	
Affected Units	SO2	NOx	voc	со	PM10	Comments
Saturate Gas Plant Heater	0.8	132.1	2.6	39.6	3.6	Emissions represent 6/1999 – 5/2001 actual emissions from fuel combustion.
LPVGO Hydrotreater Charge Htr	0.5	2.1	0.1	1.9		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
LPVGO Hydrotreater Charge Htr	3.9	17.1	1.0	16.0		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
LPVGO Hydrotreater Stripper Hti	1.8	7.9	0.5	7.3		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
HPVGO Hydrotreater Charge Htr	5.1	56.0	1.5	22.7		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
HPVGO Hydrotreater Charge Htr	5.5	66.0	1.6	24.2	2.2	Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
No. 1 SRU Thermal Oxidizer	17.3	4.7	0.3	3.9		Actual emissions for 1999-2001. SO2 based on CEMS data; others based on fuel gas input and emission factors from AP-42 Section 1.4.
No. 2 SRU Thermal Oxidizer	13.6	3.2	0.2	2.7		Actual emissions for 1999-2001. SO2 based on CEMS data; others based on fuel gas input and emission factors from AP-42 Section 1.4.
(New) FCCU Heat Recovery Units North and South	1,049.0	498.0	16.8	32.1		Emissions represent 1999 - 2000 actual emissions.
DD #2 Reactor Charge Htr	0.2	4.6	0.6	8.9		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
DD #2 Reactor Charge Htr	0.2	4.6	0.6	8.9		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.
DD #2 Stripper Reboiler	0.7	14.9	2.1	31.6		Emissions represent 6/1999 - 5/2001 actual emissions from fuel combustion.

Table 2. Baseline Actual Emissions

		actual	emissions (tons/yr)	1	
Affected Units	SO2	NOx	voc	СО	PM10	Comments
gas oil						Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil						Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil						Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil						Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil			0.	2		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil			1.	8		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil			0.	1		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
gas oil						Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
FCC gasoline			3.	7		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
FCC gasoline			6.	7		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
FCC gasoline			3.	2		Emissions represent 6/1999 - 5/2001 actual emissions from standing and working losses.
swing tank						New tank – no baseline emissions.
Distillate						
Distillate						
Distillate						
Distillate						

Table 3. Potential Emissions

				maximum	emission	ıs (tons/yr)		
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	voc	со	PM10	Comments
1-2-B-3	B018	#2 Crude Charge Htr	12.8	47.7	2.6	40.1	3.6	Maximum allowable emissions from fuel combustion assuming constant operation at maximum heat input capacity. Gas firing only.
2-23-B-3	B004	#3 Crude Unit Htr	20.8	54.3	4.3	65.2	5.9	Maximum allowable emissions from fuel combustion assuming constant operation at maximum
2-23-B-4	B005	#3 Crude Unit Htr	20.8	54.3	4.3	65.2	5.9	heat input capacity. Gas firing only.
2-26-B-2		#4 Vacuum Charge Htr	16.2	42.8	3.3	50.6	4.6	Maximum allowable emissions from fuel combustion assuming constant operation at maximum
2-23-B-6		#4 Vacuum Charge Htr	21.4	111.3	4.4	66.8	6.0	heat input capacity. Gas firing only.
2-30-B-1	B010	Saturate Gas Plant Heater	21.0	54.6	4.3	65.6	5.9	Heater may be debottlenecked. Emissions increases represent difference between maximum allowable emissions and baseline actual emissions.
2-36-B-1	B065	HF Alky Isostripper Reboiler	11.1	41.4	2.3	34.8	3.	Maximum allowable emissions from fuel combustion assuming constant operation at maximum heat input capacity. Gas firing only.
2-36-B-2		HF Alky Hot Oil Heater	2.3	8.7	0.5	7.3	0.7	Maximum allowable emissions from fuel combustion assuming constant operation at maximum heat input capacity. Gas firing

Table 3. Potential Emissions

				maximum	emissior	ns (tons/yr)	
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	voc	со	PM10	Comments
								only.
2-122	n/a	Hydrogen Generation Unit			14.5	4.6		VOC and CO from reformer vent. No components in VOC service.
2-122-B-1	n/a	Reformer Heater	1.1	104.6	9.7	70.	3 13.3	Proposed maximum allowable emissions.
2-103-B-1	B043	LPVGO Hydrotreater Charge Htr	5.8	21.7	1.2	18.	2 1.6	Maximum allowable emissions
2-103-B-2	B044	LPVGO Hydrotreater Charge Htr	5.8	21.7	1.2	18.	2 1.6	from fuel combustion assuming constant operation at maximum
2-103-B-3	B045	LPVGO Hydrotreater Stripper Htr	6.5	24.1	1.3	20.	2 1.8	heat input capacity. Gas firing sonly.
2-104-B-1	B046	HPVGO Hydrotreater Charge Htr	11.7	23.8	2.4	36.	4 3.3	Maximum allowable emissions from fuel combustion assuming constant operation at maximum
2-104-B-2	B047	HPVGO Hydrotreater Charge Htr	11.7	23.8	2.4	36.	4 3.3	heat input capacity. Gas firing only.
2-106-B-307	B042	No. 1 SRU Thermal Oxidizer	323.0	25.0	1.4	1 21.	0 3 (Maximum allowable emission
2-120-B-2	n/a	No. 2 SRU Thermal Oxidizer	323.0	25.0	1.2	21.	2.0	rates. (Total for two emission points).
2-116-B-1, 2-116-B-2	B066, B067	(New) FCCU Heat Recovery Units North and South	256.0	365.0	55.0	44	8 265.4	Emissions represent proposed maximum allowable emissions, assuming constant operation at maximum coke burn rate.
2-121-B-1	B066	DD #2 Reactor Charge Htr	7.1	11.5	1.5	22.	3 2.0	Maximum allowable emissions

Table 3. Potential Emissions

				maximum	emissior	ns (tons/yr)) 	
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	voc	со	PM10	Comments
2-121-B-2	B067	DD #2 Reactor Charge Htr	7.′	1 11.5	1.5	22.3	2.0	from fuel combustion assuming constant operation at maximum
2-121-B-3	B068	DD #2 Stripper Reboiler	11.0	17.8	3 2.3	34.4	3.′	heat input capacity. Gas firing only.
		H2 Plant Cooling Tower					0.4	Potential to emit based on 1000 gpm circulating water flow rate, 0.003% maximum liquid drift, 6000 ppmw total solids in circulating water.
		H2 Plant Emergency Flare		0.1	0.3	3.0	3	Potential to emit based on natural gas (pilot gas & purge gas) flow rate and emission factors from AP-42 Table 13.5-1
Tank 701	HJ	gas oil			51.89	9		Represents proposed maximum
Tank 702	HK	gas oil						allowable emissions from tank throughput (working) and
Tank 845	LX	gas oil						standing losses.
Tank 821	LH	gas oil						
Tank 733	IF	gas oil						
Tank 855	ME	gas oil						
Tank 81		gas oil						

Table 3. Potential Emissions

				maximi	um emissi	ons (tons	/vr)	
MAD	VEIC			- Haxiiii		0113 (10113	,,,,	
MAP Unit #	KEIS Unit #	Affected Units	SO2	NOx	voc	СО	PM10	Comments
Tank 152	FD	gas oil						
Tank 734	IM	FCC gasoline						
Tank 783	JT	FCC gasoline						
Tank 856	JV	FCC gasoline						
Tank 910	n/a	distillate						
Tank 911	n/a	distillate						
Tank 912	n/a	distillate						
Tank 913	n/a	distillate						
Tank 920	n/a	swing tank						

		Table	4. Incre	emental En	nissions Inc	reases		
MAP	KEIS			emissi	ons changes	(tons/yr)		
Unit #	Unit #	Affected Units	SO2	Nox	VOC	co	PM10	Changes
1-2	n/a	#2 Crude Unit			0.1	1		reflects change in component count
2-2	n/a	(Old) FCC Gas Con Unit			-55.6	6		reflects change in component count
2-23	n/a	#3 Crude Unit			9.9	9		reflects change in component count
2-26	n/a	#4 Vacuum Unit			3.3	3		reflects change in component count
2-103	n/a	Low Pressure VGO Hydrotreater			14.	1		reflects change in component count
2-104	n/a	High Pressure VGO Hydrotreater			89.3	3		reflects change in component count
2-109	n/a	(New) FCC Unit			8.6	5		reflects change in component count
2-110	n/a	(New) FCC Gas Con Unit			16.0)		reflects change in component count
2-121	n/a	Distillate desulfurizer #2			4.4	1		reflects change in component count
n/a	n/a	Tankage			17.4	1		reflects change in component count
Tank 910	n/a							
Tank 911	n/a							
Tank 912	n/a							
Tank 913	n/a							
1-4-B-1	B021	P-Chem Reformer Guard Case Htr	0.	.9 2	.9 0.2	2 2.	7 0	.2

							Incremental emissions increases
1-4-B-2, 3,4	B022	P-Chem Reformer Htr	2.4	8.1	0.5	7.6	0.7 based upon increase in actual
							fired duty equal to 10.7 percent of 0.3
1-4-B-7, 8	B050	Petrochem Reformer Htr	1.1	3.5	0.2	3.3	0.3 capacity.
1-44-B-1		LP CCR Charge Heater	0.9	2.9	0.2	2.8	0.2
1-44-B-2		LP CCR No. 1 Interheater	1.1	3.8	0.2	3.5	0.3
1-44-B-3		LP CCR No. 2 Interheater	0.9	2.9	0.2	2.8	0.2
1-44-B-4		LP CCR No. 3 Interheater	0.6	2.1	0.1	2.0	0.2
1-44-B-5		LP CCR Debutanizer Reboiler	0.3	1.0	0.1	1.0	0.1
							Incremental emissions increase based upon increase in actual fired duty equal to 8.1 percent of
2-35-B-1, 2	B040	C5/C6 Isomerization Heaters	1.0	3.2	0.2	3.0	0.3capacity.
2-101-B-1	B064A	Naphtha Hydrotreater Charge Heater	0.8	2.5	0.2	2.4	0.2
2-101-B-2	B064B	Naphtha Hydrotreater Stripper Reboiler	1.0	3.3	0.2	3.1	0.3
2-102-B-1A	B109	HP CCR Reactor Heater	1.8	6.1	0.4	5.7	0.5
2-102-B-1B	B110	HP CCR Reactor Heater	2.0	6.5	0.4	6.1	0.6
2-102-B-1C	B111	HP CCR Reactor Heater	1.4	4.7	0.3	4.4	0.4
2-102-B-1D	B112	HP CCR Reactor Heater	0.4	1.5	0.1	1.4	Incremental emissions increases 0.1 based upon increase in actual
2-102-B-2	B113	HP CCR Debutanizer Reboiler	0.3	1.1	0.1	1.0	fired duty equal to 10.7 percent of 0.1 capacity.

			emissions of	changes (tor	ns/yr)	
project	Comments	SO2	NOx	VOC	CO	PM10
note:	assume nonattainment NSR contemporaneous perio	od begins 7/	1/1992			
Refinery modernization project increases	See worksheet "summary"	444.20	301.95	280.84	780.37	85.54
Refinery modernization project decreases	See worksheet "summary"	-4,182.12	-1,040.55	-149.18	-807.12	-118.41
	Placed in service sometime between 10/30/1992					
	(inspection) and 2/2/1993 (operating permit application).					
	10/1993 permit application not available. "No net					
C-92-139	emissions increase" based on 8/12/1992 and					
RCC Flare Tip Replacement	10/22/1992 letters to DAQ.					
C-90-008						
a) Tanks 868, 869 & b) CTLO exchanger	Taken from 1992 Netting Spreadsheet			4.72		
C-90-078						
Amendment 1 (6 Projects in One)	Taken from 1992 Netting Spreadsheet			11.63		
	Operation commenced between 2/10/1992 (inspection -					
	construction underway) and 8/25/1992 (stack testing).					
C-90-147	Assumed no change in emission rate - no credit was					
FCC ESP amendment 2	taken for reducing PM emissions.					
C-90-171						
No. 12 Boiler amendment 1	Taken from 1992 Netting Spreadsheet CTPMLIST.WK1	22.00	118.20	0.24	32.80	4.10
	Commenced operation 7/29/1993 through 8/11/1993					
	(individual emission units, based on 8/5/1993 and					
	8/19/1993 letters to DAQ). Revised construction permit					
	issued 11/23/1993 reflects only administrative revisions,					
	no modifications. Emissions increases based on					
C-91-051	3/22/1991 and 8/22/1991 construction permit					
Distillate desulfurizer & cooling tower	applications.	37.6	40.00	36.23	35.77	5.11
	Commenced operation date not available; commenced					
	construction date 3/5/1992 (based on 3/6/1992 letter to					
C-91-057	DAQ). Emissions increase based on 1/15/1992					
Spec G-Oil Treater (revision 2)	application for revision to construction permit.			0.55		
C-91-075	Reflects PTE of three new tanks and PTE-actual for six					
Tanks 873, 874, 875	tanks undergoing a change in service			-30.67		
	Commence operation date 1/28/1994 (based on					
C-91-135	2/10/1994 letter to DAQ). Emissions changes based on					
Benzene NESHAP WWTP	1999 KEIS pg 706/708 of 720 - Column marked "Total			18.13		

			emission	s changes (tons/yr)	
project	Comments	SO2	NOx	VOC	СО	PM10
	POTENTIAL Emissions."					
C-91-136	Taken from 1999 KEIS pg 568 of 720 - Column marked					
Air Assisted Flare	"Total POTENTIAL Emissions"	0.1	3 0.	61 0.	01 0.1	5 0.01
	Commenced operation 8/12/1992 (based on 8/27/1992					
	letter to DAQ). VOC emissions increase based on					
	6/8/1992 construction permit application (revised). No					
	credit taken for any VOC emissions decrease resulting					
C-92-017	from cessation of DNO loading at					
DNO Loading Relocation	Old Naphtha Loading Rack.			5.	83	
	Commence operation date 12/7/1993. Emissions					
	increase based on 5/21/1992 letter to DAQ (requesting					
	revision to construction permit). Increase includes PTE					
	of 3 new tanks, fugitive components associated with all					
	7 tanks covered by construction permit, and 2-year					
	actual emissions of 14 tanks (14,					
C-91-164	18, 24, 42, 62, 63, 66, 67, 68, 101, 102, 136, 137, 164)					
Tanks 48, 49, 55, 56	being removed concurrently.			-1.	73	
	Commence operation date 10/28/1994 (based on					
	11/2/1994 letter to DAQ). Emissions increase based on					
	5/21/1992 letter to DAQ (requesting revision to					
C-91-164	construction permit). Increase includes PTE of 2 new					
Tanks 34, 43	tanks only.			0.	36	
	Commence operation date 7/29/1995 (based on					
	7/31/1995 letter to DAQ). Emissions increase based on					
	5/21/1992 letter to DAQ (requesting revision to					
C-91-164	construction permit). Increase includes PTE of new					
Tanks 32	tank only.			4.	61	
	Commenced operation 12/21/1992 (based on					
	12/28/1992 letter to DAQ). Emissions increase based					
	on 5/20/1991 construction permit application, reflects					
C-92-029	PTE of new tank and 2-year actual emissions of Tank					
Tank 883	787 (being replaced).			-3.	06	
C-91-175	Commenced operation 12/21/1992 (based on					
Tank 884	12/28/1992 letter to DAQ). Emissions increase			-6.	38	

	Table 3. Netting Analyses		emissions of	changes (to	ns/yr)	
project	Comments	SO2	NOx	voc	CO	PM10
	includes PTE of new tank and 2- year actual emissions					
	of Tank 788 (being replaced).					
	Commence operation date not available, but ~					
	11/5/1992 (submittal date for construction permit					
	application for fired duty increase at #5 crude charge					
n/a (1992)	heater, at which time installation was complete but unit					
retrofit #4 boiler with low-NOx burners	was not yet operational)		-738.00)		
	Commence operation date not available (construction					
C-92-009	permit issued 2/21/1992). Emissions increase based					
Additive Tank 891	on 12/18/1991 construction permit application.			1.18	3	
	1-44-B-1 through B-4 heaters commenced operation on					
	9/28/1993 and B-5 heater on 10/6/1993 (based on					
	10/8/1993 letter to DAQ). CCR Unit (fugitives)					
	commenced operation on 9/17/1993 (based on					
	9/20/1993 letter to DAQ). Emissions increases based					
	on revised construction permit issued 10/11/1993					
	(except for CO - no limits in permit - based on KEIS)					
	(initial permit issued 2/26/1992 was superseded). No					
C-92-033	credit taken for shutting down fixed-bed reformer (VOC	00.45		40.00	540	
Petrochem CCR Unit	emissions) or heater 1-4-B-1.	32.15	39.96	40.00	51.94	14.99
	Commenced operation on construction permit issuance					
	date. Emissions increases based on 8/22/1995 revised					
0.00	construction permit and 10/26/1994 application					
C-92-033	(construction permit issued 2/26/1992 was				0.00	
Petrochem CCR Unit	superseded).	7.76	-0.05		0.62	4
	Commence operation 1/11/1995 (based on 1/20/1995					
	letter to DAQ). Commenced construction 2/1/1993					
	(based on 2/10/1993 letter to DAQ). (Modification					
	involved tie-in of several relief vents over ~2-year period.)	1				
6 00 000	Zero emissions increase, based on 1/27/1988 permit					
C-92-062	application.					
Petrochem and South Area flare						

	Table 5. Netting Analyses	emissions changes (tons/)				
project	Comments	SO2	NOx	VOC	co	PM10
	Commenced operation 1/12/1994 (based on 1/17/1994					
C-92-096	letter to DAQ). Emissions increases based on 5/6/1992					
Furfural slop tanks 104, 882	construction permit application.			5.95	5	
	Operation commencement date not available;					
	construction permit issued 9/29/1992. VOC emissions					
C-92-132	increase based on 2/21/1991 construction permit					
RCCS Ram Oil System	application.			5.13	3	
·	Operation commencement date not available;					
	construction permit issued 11/24/1992. VOC emissions					
	increase based on 8/5/1992 construction permit					
	application, assuming 6 million gallons per year for					
C-92-140	each tank, and including fugitives. No credit taken for					
DNO storage tanks 138, 139	shutdown of Tank 187.			7.22	2	
	Based on revised valve count (12/10/1992 letter to					
C-92-142	DAQ, requesting revocation of construction permit;					
Dubbs off gas compressor spare	request was denied).			1.44	1	
	Commence operation date 5/20/1993 (based on					
C-93-040	5/21/1993 letter to DAQ). Emissions increases based					
contractor fuel tanks	on 3/16/1993 construction permit application.			0.2		
	Commenced operation 9/3/1994 through 9/16/1994 (for					
	individual emission units). Emissions increases based					
C-93-116	on 9/13/1993 letter to DAQ requesting revisions to					
SDA Unit Restart	construction permit.	11.73	39.99	39.64	15.20	2.18
C-93-182						
Refinery vehicle gasoline tank	Based on construction permit application.			0.47	1	
	Commenced operation 7/12/1996 (based on 7/18/1996					
	letter to DAQ). VOC emissions change based on					
0.04.044	7/27/1993 construction permit application. Other					
C-94-014	increases based on 11 MMBtu/hr heat input and AP-42			10.4	7 4 0	- 00-
Solvent loading thermal oxidizer	Section 1.4.	0.03	3 4.82	-16.47	4.0	0.37
S-94-181	Project scope involved replacing 10 existing tanks with					
replace 10 tanks	10 tanks having the same ID numbers. (Necessary to			9.42	4	

		emissions changes			ons/yr)		
project	Comments	SO2	NOx	VOC	СО	PM10	
	accommodate fire code.) VOC emissions increase represents PTE-to-actual, based on 9/13/1994 permit application.						
S-95-006	Commence operation 7/1/1996 (based on 7/2/1996 letter to DAQ). Emissions increase based on 6/19/1995 construction permit application, reflects post-change						
Tank 734 to gasoline service	PTE and pre-change actual (in diesel service).						
S-95-037 Lube vacuum tail gas recovery system	Commence operation 12/28/1995 (based on 1/3/1996 letter to DAQ). VOC emissions increase based on 9/29/1994 construction permit application.			4.62) -		
S-95-120 Tank 64 replacement	Commence operation 9/26/1995 (based on 10/11/1995 letter to DAQ). Emissions increase based on 4/13/1995 construction permit application, reflects PTE of new tank and actual emissions of old tank. No change in emission rate for any PSD/NSR-regulated			-0.21			
S-95-152 CCR chlorination agent change	pollutant. Phase-out of carbon tetrachloride mandated by Title VI of Clean Air Act. Does not change "normal operation" of the unit.						
S-95-145 Replace #4 vacuum heaters	Commence operation date not available; construction permit issued 7/31/1995. Emissions changes reflect installation of heater 2-26-B-2 and shutdown of 2-1-B-1 and 2-23-B-1, based on 6/5/1995 construction permit application.	10.61	-3.6	5 -5.0	15.78	1.9	
S-95-172 Dubbs area vacuum tail gas recovery	6/19/1995 construction permit application includes no emission estimates other than VOC from new piping.			4.62	2		
S-96-091 #5 crude charge heater duty increase	Based on 1/26/1996 construction permit application.		69.00			21.94	
S-95-213 New north area CCR heaters	Construction permit application 2/16/1993 for increasing fired duties		124.00				

			emissions	ns changes (tons/yr)		
project	Comments	SO2	NOx	VOC	CO	PM10
S-96-016	VOC emissions increased based on 12/14/1995					
propylene/propane bullets relocation	construction permit application.					
				6.60)	
	Commenced operation 11/8/1996. Emissions increase					
	based on 12/15/1995 construction permit application,					
	reflects prereconstruction actual emissions and post-					
S-96-018	reconstruction PTE.					
Tank 355				-3.97	7	
S-96-207				-5.9		
Cumene unit expansion	(see 2/13/1996 permit application)	9.0	0 39	9.9 32.00	11.00	o
	Project scope involved replacing 4 existing tanks (5, 6,					
	112, 113) with 4 new tanks (26, 195, 196, 197).					
S-96-242	Emissions increase represents PTE-to-actual, based					
Toluene tanks change in service	on permit application.					
				3.86	5	
S-96-251						
Add loading arms at Viney Branch	Emissions increases based on permit application.			4= 4		
Note: assume PSD (contemporaneous period begins 4/1/1997; projects ab	ove here a	ro not cour	17.40		
S-97-012	Emissions increases based on 11/4/1996 permit	ove nere a	e not coul	ited for F3D		
Tank 902 Isomerate charge	application. Commenced operation 3/11/1998.			5.43	3	
S-98-057	application. Commonicou operation of 11/1000.			0.10		
Ethanol storage tank at Viney Branch	Emissions increases based on permit application.			2.56	3	
thanor storage tark at viney Branon	VOC emissions increases from new piping			2.00		
S-98-088	components, based on 8/31/1998 construction permit					
Hydrogen coalescers	application.			7.13	3	
	No change in emission rate for any PSD/NSR-regulated					
	pollutant. Phase-out of carbon tetrachloride mandated					
S-98-089	by Title VI of Clean Air Act. Does not change "normal					
Change chlorinating agent at Isom Unit	operation" of the unit.			0.00		

	Table 5. Netting Analyses		emissions changes (tons/yi		ns/yr))	
project	Comments	SO2	NOx	VOC	CO	PM10	
	VOC emissions increase stated in 5/12/1999						
	construction permit application. No credit taken for any	,					
S-99-052	decrease resulting from removal of components						
HF Alky flare drum relocation	associated with existing underground drum.			3.15	5		
	VOC emissions increase based upon 10/19/1999						
S-00-007	permit application. Commence operation date not						
Tank 733 modification	known.			3.76	5		
	Commenced operation 3/1/2000 (based on 3/3/2000						
	letter to DAQ). RCC CO boiler increases calculated as						
S-00-011	difference between 1997-1999 actual and 1999-2001						
RCC regenerator	actual. Increases reflect 11/2001 revision to permit.	0.89	8.34		22.24		
WO9902020							
#2 Refinery railcar loading rack				-0.80)		
N/A							
Wastewater plant modifications				4.64	ļ.		
N/A							
LEP gas compressor				4.99)		
WO9902871							
Asphalt cooling NTE				2.13	3		
N/Also-octene unit				5.38	3		
WO990761							
Tank 144 change of service				1.18	3		
WO990755							
New fuel gas vent drum 2-66-F-13				1.20)		
WO9900756							
Piping from 894 tank to #3 crude unit				1.87			
WO990842KY							
Barge loading line relief				1.60)		
WO990765							
Remove Tank 65 IFR				10.16	5		

	Tuble of Netting Analyses	emissions changes (tons/yr)				
project	Comments	SO2	NOx	VOC	CO	PM10
WO990856						
AC-5 closed-loop sampler for lube vac unit				0.03	3	
WO990770						
Tank 122 - add 3 valves				0.05	5	
WO000373						
Pitch unit piping installations				0.52	2	
WO000162						
Alky depropanizer to Alky regen				0.11		
WO000395						
2-30-F-11 depropanizer relief valve				0.21		
WO000333						
Spillback line from 701/702 tank pumps				0.08	3	
WO R09-1191						
New bleeder at 110-E-25				0.02	2	
WO990015						
South end light oil tank farm - underground						
lines				0.68	3	
WO003785						
Route depropanizer sidedraw to D12				0.08	8	
WO000028				0.04		
New tank 105 in slurry/fuel oil service				0.31		
WO000081				0.07	,	
MEK filters				0.37		
WO000457High sulfur isobutane at sat gas plant				0.06		
				0.00)	
WO000473 Closed loop sampler at #1 SRU				0.12	,	
WO00470				0.12	-	
Closed loop sampler at Pchem fuel gas				0.18		
WO00469				0.10	1	
Closed loop sampler at MEK unit				0.05		
Closed loop sampler at MER unit				0.00	1	

	emissions changes (tons/yr)						
project	Comments	SO2	NOx	VOC	CO	PM10	
WO000467							
Closed loop sampler at south area fuel gas				0.11			
WO000471							
Closed loop sampler at HP CCR				0.12	2		
WO000472							
Closed loop sampler at VGO				0.09	9		
WO000468							
Closed loop sampler at RCC gas con reflux				0.09	9		
WO000117							
Closed loop sampler at RCC gas con fuel				0.08	3		
WO000459							
Drain lines on KOH heater				0.12	2		
WO00081							
Pitch unit pump seals				0.34	1		
n/a							
Add 4 diesel loading arms				0.28	3		
WO9902798							
Cumene unit relief system capital				0.23	3		
WO359133							
Cumene unit relief system expense				0.08	3		
WO1049133							
VGO relief system expense				0.08	3		
WO289133							
ADS/CTLO unit relief system expense				0.23	3		
WO9902631							
Cooled sat gas pumparound system				0.51			
WO9902751							
Add flow meter to 2-106-B-301 side nozzle				0.08	3		
W0000407Delegation of lab = 44 to 44				0.00			
WO000497Relocation of lube 41-tc-44				0.03	3		
WO980503				0.44			
Block and bleed valves in lube vac tower				0.12	4		

		emissions changes (tons/yr)				
project	Comments	SO2	NOx	VOC	CO	PM10
WO9902961						
Flush line to caustic precipitator				0.02	2	
N/A						
implement 40 CFR 63 subpart H LDAR				-256.08	3	
TOTAL		-3,605.92	-730.26	-64.63	-4.50	-32.56

III. REGULATORY APPLICABILITY AND FEDERALLY ENFORCEABLE CONDITIONS AND LIMITATIONS

A. PSD

The Kentucky PSD program, 401 KAR 51:017, applies to construction of a major source or major modification in an area that is not designated nonattainment for the pollutant in question. This program meets the federal PSD program requirements set forth at 40 CFR 51.166, as required by part c, Title I of the Clean Air Act. The area in which the Catlettsburg refinery is located, in Boyd County, is either undesignated or is designated attainment for all pollutants other than SO₂.

Applicability of the PSD regulations is not triggered for the Refinery Modernization Project because no significant net emissions increase will result. The net emissions increases for all PSD-regulated pollutants, and the corresponding "significant" levels, are shown in Table 6. The emissions increase calculations include emissions from new and modified emissions units as well as other affected emissions units upstream and downstream of the new and modified equipment. Consistent with current U.S. EPA policy, emissions increases for all modified and debottlenecked emissions units are calculated using a past-actual-to-future-potential methodology. For PM/PM10, NOX, CO, and VOC emissions, netting analyses were performed, including all contemporaneous emissions increases and decreases. For all pollutants, the net emissions increases are less than significant (in fact, for VOC, SO₂, and NOX, the project will result in significant decreases). Construction under the Refinery Modernization Project commenced after January 6, 2002, so a five-year contemporaneous period is used for PSD netting analyses consistent with 401 KAR 51:017, Section 1, paragraph (30)(b).

B. Nonattainment NSR

The Kentucky nonattainment NSR program, 401 KAR 51:052, applies to construction of a major source or major modification in an area that is designated nonattainment for the pollutant in question. This program meets the federal nonattainment NSR program requirements set forth at 40 CFR 51.165, as required by part d, Title I of the Clean Air Act. The area in which the Catlettsburg refinery is located, in Boyd County, is designated nonattainment for SO₂.

Applicability of the nonattainment NSR regulations is not triggered for the Refinery Modernization Project because no significant net emissions increase will result. The net emissions increase and the corresponding "significant" level for SO₂ are shown in Table 6. A ten-year contemporaneous period is used for the nonattainment NSR netting analysis consistent with 401 KAR 51:052, Section 1, paragraph (19)(c).

TABLE (CITINATA	A DAY OF DOD AIGD	A DDT TO A DTT TOTAL	T/E 03 001 (D · · 1)
IAKIRA		ARY OH PSD/NSR	APPLICARILITY	VF-02-001 (Revision 1)

Pollutant	Net Emissions Increase (tons/yr)	Significant Thresholds (tons/yr)	PSD or NSR?	PSD/NSR apply?
PM	-33	25	PSD	No
PM-10	-33	15	PSD	No
SO_2	-3,605	40	NSR	No
NO_X	-730	40	PSD	No
VOC	-64	40	PSD	No
CO	-4	100	PSD	No

C. Marathon Ashland Petroleum / U.S. EPA Global NSR Settlement

Catlettsburg Refining and its parent company, Marathon Ashland Petroleum, entered into a consent decree with U.S. EPA in May 2001. This consent decree requires the implementation of certain environmental measures at the Catlettsburg refinery. In addition, the consent decree discourages Catlettsburg Refining from relying on certain of the emission reductions, required under the consent decree, in PSD or nonattainment NSR netting analyses.

Catlettsburg Refining has represented to the Division that the netting analyses described herein do not rely on emission reductions, the use of which is discouraged under the consent decree. Specifically, the following emission reductions are not relied upon in the PSD and nonattainment NSR netting analyses for the Refinery Modernization Project:

- ?? The SO₂ emission reduction of 195.5 tons per year from the #2 Crude Charge Heater (Unit No. 1-2-B-3). This reduction will result from elimination of oil firing, which is required under the consent decree.
- ?? The NO_X emission reductions of 276.2 tons per year from the #3 Crude Charge Heaters (Unit Nos. 2-23-B-3 and 2-23-B-4) and 97.6 tons per year from the HPVGO Hydrotreater Charge Heaters (Unit Nos. 2-104-B-1 and 2-104-B-2). These reductions will result from retrofitting with low-NO_X burners, which is required under the consent decree.
- Provided Pro
- Recovery Units (Nos. 2-116-B-1 and 2-116-B-2). The permit limits the SO₂ emissions from these units to 256.0 tons SO₂ per year. As compared to past actual emissions of 1,049.0 tons SO₂ per year, this limit will require an emission decrease of at least 793.0 tons SO₂ per year. The consent decree would require implementation of emission reduction measures that would result in allowable SO₂ emissions of 681.0 tons per year. Thus, emission reductions of 368.0 tons SO₂ per year are required by the consent decree and are discouraged from being relied upon under the consent decree.
- ?? The NO_X emission reduction of 261.0 tons per year from the existing RCC Unit (No. 2-109) and Heat Recovery Units (Nos. 2-116-B-1 and 2-116-B-2). This reduction will result from implementation of several measures that are required under the consent decree.

- ?? The total SO₂ emission reduction that is required by this permit and discouraged from being relied upon under the consent decree, as described above, is 3,618.9 tons per year. The net SO₂ emissions decrease shown in Table 5 is 3,599.6 tons per year. Thus, without considering the emission reductions that are required by the consent decree, the net SO₂ emissions increase for the Refinery Modernization Project would be 19.3 tons per year.
- The total NO_X emission reduction that is required by this permit and discouraged from being relied upon under the consent decree, as described above, is 844.0 tons per year. The net NO_X emissions decrease shown in Table 5 is 945.3 tons per year. Thus, without considering the emission reductions that are required by the consent decree, the net NO_X emissions decrease for the Refinery Modernization Project would be 101.3 tons per year.

D. NSPS

Federal New Source Performance Standards (NSPS) are required under section 111 of the federal Clean Air Act and are codified at 40 CFR part 60. Several NSPS regulations are potentially applicable to emissions units that are affected by the Catlettsburg Refinery Modernization Project.

The NSPS for Petroleum Refineries, 40 CFR 60 subpart J, is applicable to the new FCC Unit (ID No. 2-109) and to several fuel gas combustion devices at the Catlettsburg refinery. Where applicable, this regulation is noted on the DEP7007V permit application form included in Appendix A.

NSPS subpart J is not applicable to the Hydrogen Generation Unit Reformer Heater (ID Nos. 2-122-B-1) because this unit combusts only natural gas.

NSPS subpart J is applicable to the Sulfur Recovery Plant (ID Nos. 2-106, 2-107, 2-118, 2-119, and 2-120). This regulation limits SO_2 emissions to 250 ppmv on a dry, oxygen-free basis.

The NSPS for Volatile Organic Liquid Storage Vessels, 40 CFR 60 subpart Kb, is applicable to the new Tank 920 and to several existing tanks, as noted in the Kentucky DAQ air quality permit application form DEP7007V. It is worth noting that several other tanks, including Tank Nos. 152, 701, 702, 783, 821, and 845, are not subject to any NSPS regulation because these tanks have not been constructed, reconstructed, or modified after June 11, 1973. The Refinery Modernization project will not involve any modifications to these tanks, although the tanks may undergo minor changes such as being insulated or having new nozzles installed.

The NSPS for Equipment Leaks of VOC in Petroleum Refineries, 40 CFR 60 subpart GGG, is applicable to several process units at the Catlettsburg refinery. Three new compressors in VOC service are being installed as part of the Refinery Modernization Project, each of which is a separate affected facility for NSPS applicability purposes. Where applicable, NSPS subpart GGG is noted on the DEP7007V permit application form included in Appendix A. It is worth noting that NSPS subpart GGG is not applicable to the Hydrogen Generation Unit (ID No. 2-122) because this unit does not include any equipment in VOC service, as that term is defined at 40 CFR 60.481.

The NSPS for VOC Emissions from Petroleum Refinery Wastewater Systems, 40 CFR 60 subpart QQQ, will apply to the new drain system associated with the Hydrogen Generation Unit (ID No. 2-122). This drain system will comply with the provisions of 40 CFR 60.692-2. Wastewater from this drain system will be conveyed to the refinery's existing NESHAP-compliant wastewater system.

NSPS subpart Dc is applicable to the HF Alky Unit Hot Oil Heater (ID No. 2-36-B-2). The SO₂ and PM emission standards under subpart Dc are not applicable because this unit will not burn coal, oil, or wood.

The NSPS for Volatile Organic Liquid Storage Vessels, 40 CFR 60 subpart Kb, is applicable to the new Tanks 910, 911, 912, 913, and 920.

E. PRE-1990 NESHAP

National Emission Standards for Hazardous Air Pollutants (NESHAP) promulgated prior to the Clean Air Act Amendments of 1990 were established as risk-based standards (post-1990 NESHAP are technology-based standards and are discussed in Section 3.4 of this permit application).

The NESHAP for Benzene Waste Operations, 40 CFR 61 subpart FF, is applicable to all petroleum refineries, including the Catlettsburg refinery. The Refinery Modernization Project will not impact the manner or extent to which this regulation applies to the Catlettsburg refinery. The Catlettsburg refinery will continue to comply with the standards under 40 CFR 61.342(e). No new benzene-containing waste streams requiring control under 40 CFR 61.342(c)(1) will be generated by the Refinery Modernization Project.

F. MAXIMUM ACHIEVABLE CONTROL TECHNOLOGY

NESHAP standards promulgated subsequent to the Clean Air Act Amendments of 1990, as required by § 112(d) of the Act, are generally referred to as Maximum Achievable Control Technology (MACT) standards. These standards apply to major sources of HAP, including the Catlettsburg refinery.

The Catlettsburg refinery is subject to the MACT standard for Petroleum Refineries, 40 CFR 63 subpart CC. This regulation includes emission standards for miscellaneous process vents, storage vessels, wastewater, equipment leaks, gasoline loading racks, and marine vessel tank loading operations. The Catlettsburg refinery is an existing source and is subject to the emission standards for existing sources in each of these emissions unit subcategories. The Refinery Modernization project will have little impact on the manner and extent to which subpart CC is applicable. In particular, it is worth noting that all process units at the Catlettsburg refinery will continue to be regulated, collectively, as an existing affected source.

The only new process unit, the Hydrogen Generation Unit (ID No. 2-122), will not have the potential to emit 10 tons per year of any HAP or 25 tons per year of HAPs in total. Thus, under §63.640(i), the Hydrogen Generation Unit is treated as a part of the existing affected source. The Reformer Vent is

specifically excluded from the definition of "miscellaneous process vent" at §63.641 and, thus, is exempt from the MACT emission standards.

In addition, the modifications being made to existing process units will not constitute reconstruction (which would require the addition of components with a fixed capital cost exceeding 50 percent of the fixed capital cost that would be required to construct a comparable new refinery). Thus, under §63.640(j), these modified units will continue to be regulated as an existing affected source.

Other MACT standards may impact the refinery in the future. In particular, the standard for catalytic cracking units, catalytic reforming units, and sulfur plants is likely to be promulgated in 2001 and to be codified at 40 CFR 63 subpart UUU. The impacts of any future MACT standards, if any, will be addressed once the standards become effective.

The federal *Case-by-Case MACT* rule, codified at 40 CFR 63.40 through 63.44 and incorporated by reference at 401 KAR 63:105, implements § 112(g) of the Clean Air Act, as amended. This rule applies to new or reconstructed major sources of HAP that are not covered by a source category MACT standard. The Refinery Modernization Project will not involve any such construction or reconstruction.

G. KENTUCKY NEW SOURCE STANDARDS

Several of the emission standards set forth at 401 KAR Chapter 59 are applicable to the Catlettsburg refinery and to the Refinery Modernization Project. These include the following:

- 401 KAR 59:015, "New indirect heat exchangers," is applicable to the new Reformer Heaters (ID Nos. 2-122-B-1) and several existing heaters, as noted in the Kentucky DAQ air quality permit application form DEP7007V included in Appendix A. It is worth noting that this regulation is not applicable to the No. 3 Crude Unit Charge Heaters (ID Nos. 2-23-B-3 and 2-23-B-4) because these heaters have not been constructed or modified after August 17, 1971. The Refinery Modernization Project will not involve any modification (as that term is defined at 401 KAR 59:001) to these heaters.
- 401 KAR 59:046, "Selected new petroleum refining processes and equipment," is applicable to process unit turnarounds and to vacuum-producing systems throughout the refinery.
- 401 KAR 59:050, "New storage vessels for petroleum liquids," is applicable to the new Tank 920 and to several existing tanks, as noted in the Kentucky DAQ air quality permit application form DEP7007V. It is worth noting that several other tanks, including Tank Nos. 152, 701, 702, and 783, are not subject to this regulation because these tanks have not been constructed or modified after April 9, 1972. The Refinery Modernization Project will not involve any modification to these or any other storage vessels.
- 401 KAR 59:105, "New Process Gas Streams," includes emission limitations for CO, H2S, and SO₂ for process gas streams not otherwise covered by regulations under Chapter 59. The CO and SO₂ regulations are not applicable to any gas streams affected by the Refinery Modernization Project. The H2S limitation is applicable to several process gas streams, as noted in the Kentucky DAQ air quality

permit application form DEP7007V. Compliance with the applicable H2S emission limitation is achieved by routing the process gas streams to sulfur recovery plants and combustion devices.

CREDIBLE EVIDENCE:

This permit contains provisions that require that specific test methods, monitoring or recordkeeping be used as a demonstration of compliance with permit limits. On February 24, 1997, the U.S. EPA promulgated revisions to the following federal regulations: 40 CFR Part 51, Sec. 51.212; 40 CFR Part 52, Sec. 52.12; 40 CFR Part 52, Sec. 52.30; 40 CFR Part 60, Sec. 60.11 and 40 CFR Part 61, Sec. 61.12, that allow the use of credible evidence to establish compliance with applicable requirements. At the issuance of this permit, Kentucky has not incorporated these provisions in its air quality regulations.